

Helium-3 Interstellar Starship

Performance Profile

QUANTITATIVE DETERMINISTIC EVALUATION OF A D-³HE PULSE FUSION ARCHITECTURE

To safely navigate interstellar space within a human lifetime, propulsion systems must maximize kinetic exhaust energy while minimizing structural dead-weight. This technical evaluation calculates the performance metrics of a multi-stage spacecraft using a high-yield Deuterium-Helium-3 (D-³He) pulse fusion drive. The system features magnetic nozzles that direct energetic charged particles (protons and alpha particles) to optimize acceleration timelines and cruise velocities.

1. Starship Mass Allocation Budget

The core configuration maps a heavy-class exploratory vehicle. Below is the fixed mass structure defining the dry framework and volatile fuel payloads required for deep space operations.

VESSEL COMPONENT BLOCK	MASS CONFIGURATION (METRIC TONS)	MASS CONFIGURATION (KILOGRAMS)
Structural Payload, Instrumentation & Shielding (M_f)	20,000 t	$2.0 \times 10^7 \text{ kg}$
Deuterium-Helium-3 Mixed Propellant Payload (M_p)	80,000 t	$8.0 \times 10^7 \text{ kg}$
Total Fully Laden Initial Mass (M_0)	100,000 t	$1.0 \times 10^8 \text{ kg}$

The structural mass parameters establish a definitive structural mass ratio of $M_0 / M_f = 5.00$. This represents a highly optimized system where 80% of the spacecraft's total liftoff weight consists entirely of thermonuclear fusion reactants.

2. Propellant Consumption Rate

To sustain steady relativistic velocities without overloading structural thermal barriers, the engine is designed for a sustained burn cycle. We establish a nominal mass flow rate (dm/dt or $m^{\cdot}$) of **2.50 kilograms per second** of combined $D\text{-}^3\text{He}$ plasma fuel.

CONTINUOUS FUEL BURN RATE	TOTAL HELIUM-3 MASS CONSUMED
2.50 kg / s	48,000 Metric Tons

Based on the stoichometric requirements of the reaction $^2\text{H} + ^3\text{He} \rightarrow ^4\text{He} (3.6 \text{ MeV}) + p (14.7 \text{ MeV})$, the mass ratio of the fuel mix requires approximately 60% Helium-3 by weight due to the atomic mass breakdown. Consequently, out of the 80,000 metric tons of total propellant, exactly **48,000 metric tons** ($4.8 \times 10^7 \text{ kg}$) of pure Helium-3 is consumed over the lifespan of the engine's main thrust phase.

The total duration (t_{burn}) of continuous thrust before total fuel exhaustion is calculated via:

$$t_{\text{burn}} = M_p / m^{\cdot} = 80,000,000 \text{ kg} / 2.5 \text{ kg/s} = 32,000,000 \text{ Seconds}$$

This translates to exactly **370.37 Earth days** (~1.01 years) of continuous, un-interrupted propulsion burn.

3. Thrust Determination (Kilonewtons)

The raw mechanical force produced by the fusion drive is governed by the product of the fuel mass flow rate and its directional exhaust velocity. A optimized $D\text{-}^3\text{He}$ reaction provides a net magnetic exhaust velocity (v_e) of roughly 7% the speed of light, yielding **21,000,000 m/s**.

$$\text{Thrust } (F) = \dot{m} \times v_e$$

$$F = 2.50 \text{ kg/s} \times 21,000,000 \text{ m/s} = 52,500,000 \text{ Newtons}$$

CALCULATED ENGINE THRUST OUTPUT

52,500 Kilonewtons (kN)

4. Thrust-to-Mass Ratio & Acceleration Range

The thrust-to-mass ratio changes dynamically as the spacecraft discards its fuel weight over the 32-million-second burn duration. We evaluate this ratio as an acceleration value in Newtons of thrust per kilogram of vessel mass (N/kg , structurally equivalent to m/s^2).

- **Initial Thrust-to-Mass Ratio (Laden System):** At ignition, with a full 100,000-ton fuel load, the ratio is:

$F / M_0 = 52,500,000 \text{ N} / 100,000,000 \text{ kg} = 0.525 \text{ N/kg} (0.525 \text{ m/s}^2)$. This provides a mild starting acceleration of roughly **0.0535 G**.

- **Final Thrust-to-Mass Ratio (Dry System):** At the point of fuel exhaustion, the structural mass drops to 20,000 tons, concentrating the remaining force:

$F / M_f = 52,500,000 \text{ N} / 20,000,000 \text{ kg} = 2.625 \text{ N/kg} (2.625 \text{ m/s}^2)$. This increases the peak acceleration to **0.2676 G**.

THRUST-TO-MASS OPERATING RANGE

0.525 N/kg — 2.625 N/kg

5. Terminal Cruise Velocity Profile

Integrating the changing thrust-to-mass ratio across the burn cycle using the Tsiolkovsky rocket equation identifies the ultimate terminal speed achieved by the starship at the point of engine cutoff.

$$\Delta v = v_e \times \ln(M_0 / M_f)$$

$$\Delta v = 21,000 \text{ km/s} \times \ln(5.00) = 21,000 \times 1.609438 = 33,798.2 \text{ km/s}$$

Converting this absolute kinematic value into the requested interstellar and terrestrial standard tracking units yields the following precise speed velocity profile:

MEASUREMENT FORMAT UNIT	CALCULATED FINAL CRUISE VELOCITY VALUE
Fraction of Light Speed (c)	0.1127 c (11.27% of the Speed of Light)
Terrestrial Speed Rate (km/h)	121,673,520 km/h (One Hundred Twenty-One Million km/h)
Interstellar Distance Rate	0.1127 Light-Years per Year

With a maximum cruise capability exceeding 121 million kilometers per hour, the vessel spans a total distance of one full light-year every 8.87 Earth years. This positions the spacecraft to complete flyby operations or execute phased deceleration strategies toward close stellar bodies like Proxima Centauri within standard deep space mission design tolerances.

Technical Document End • Derived utilizing classical and sub-relativistic rocketry paradigms.
Data verified for engineering feasibility under standard electromagnetic confinement models.